

Wed.	(C 21.6-7,.9) 1.3.4-1.3.5, 1.5.2-1.5.3, 5.3.1-.3.2 Div & Curl B	
Fri.	(C 21.6-7,.9) 5.3.3-.3.4 Applications of Ampere's Law	
Mon.	1.6, 5.4.1-.4.2 Magnetic Vector Potential	HW8
Wed.	5.4.3 Multipole Expansion of the Vector Potential	
Thurs.		
Fri.	Review	

Memory Lane: Electrostatics

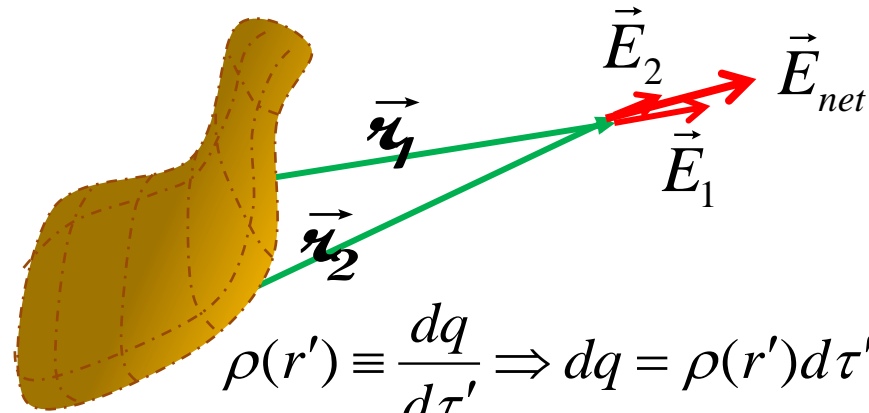
Field of charge distributions

$$\vec{E}_1(\vec{r}) = \frac{1}{4\pi\epsilon_0} \frac{q_1}{r_1^2} \hat{r}_1$$

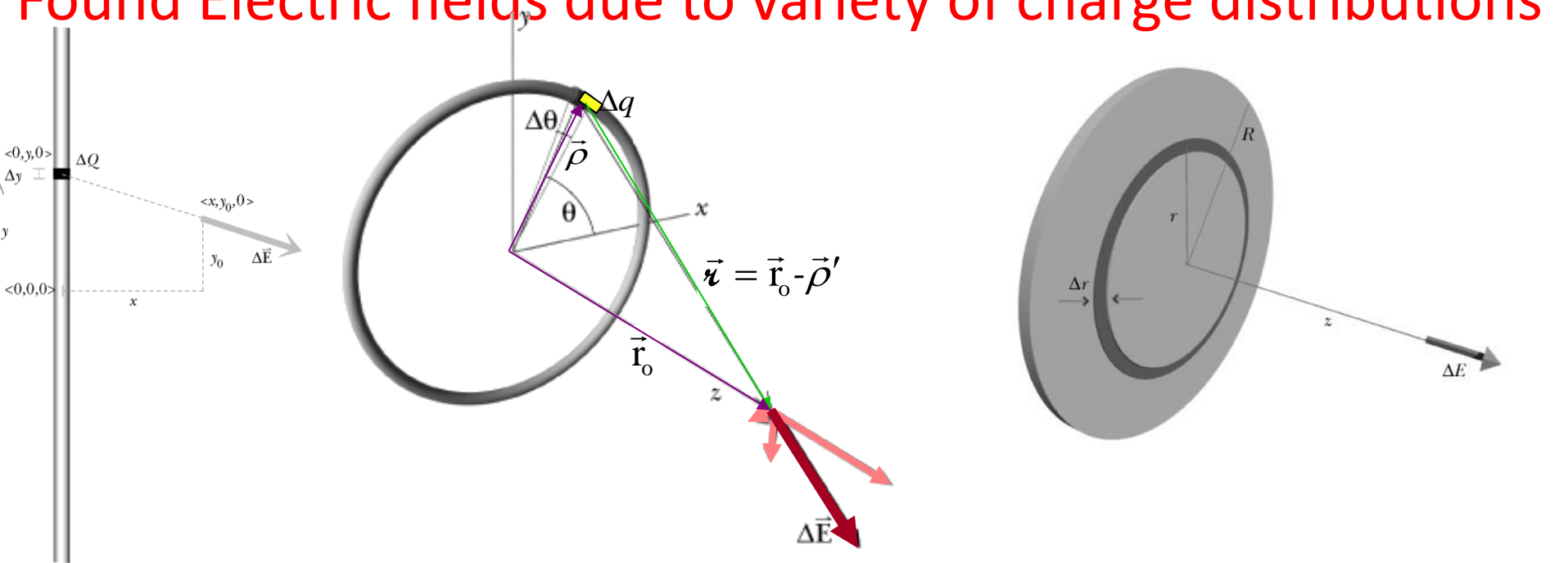
$$\vec{E}(\vec{r})_{net} = \sum_{i=1} \frac{1}{4\pi\epsilon_0} \frac{q_i}{r_i^2} \hat{r}_i \xrightarrow{\lim_{q \rightarrow dq}} \int_{charge} \frac{1}{4\pi\epsilon_0} \frac{\hat{r}}{r^2} dq$$

$$\rho(r') \equiv \frac{dq}{d\tau'} \Rightarrow dq = \rho(r') d\tau'$$

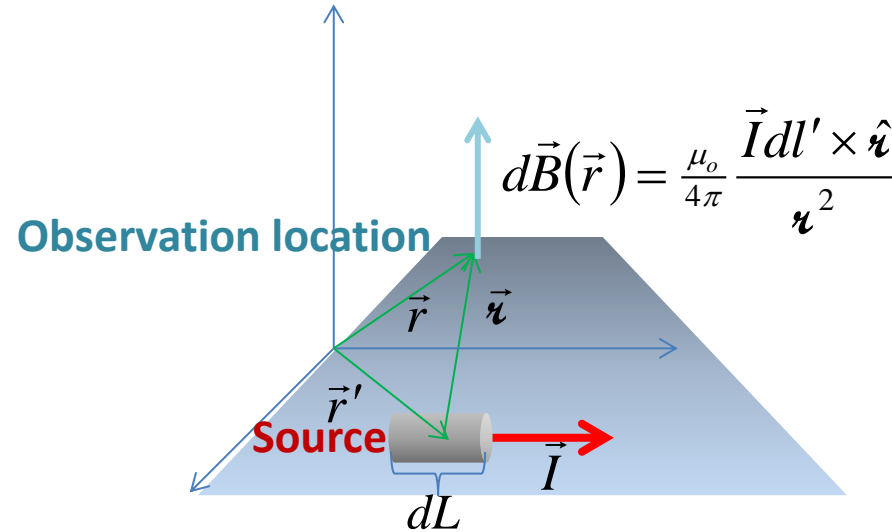
$$\vec{E}(\vec{r}) = \int \frac{1}{4\pi\epsilon_0} \frac{\hat{r}}{r^2} \rho(\vec{r}') d\tau'$$



Found Electric fields due to variety of charge distributions



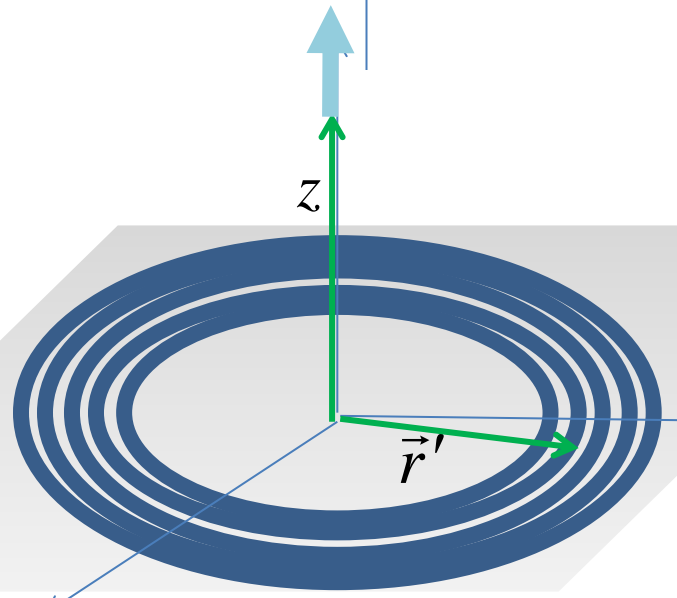
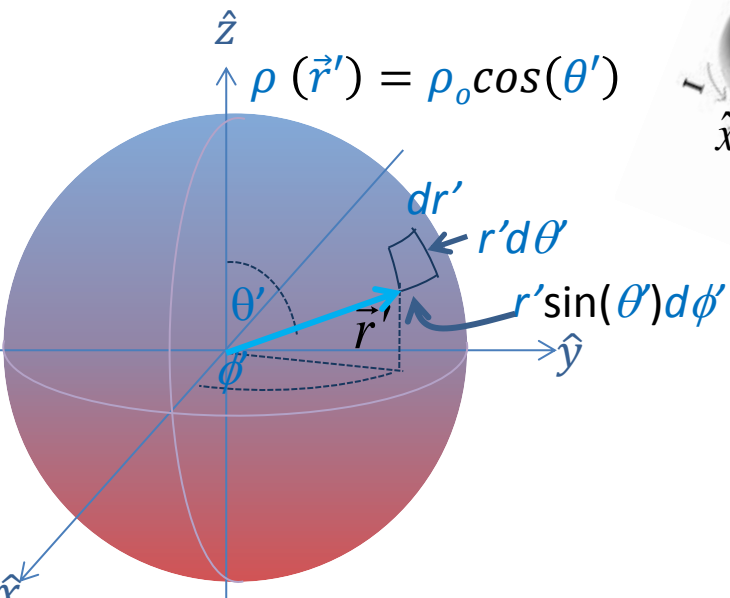
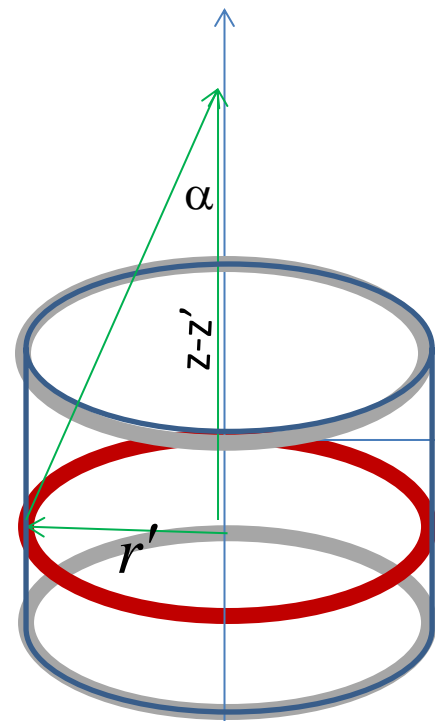
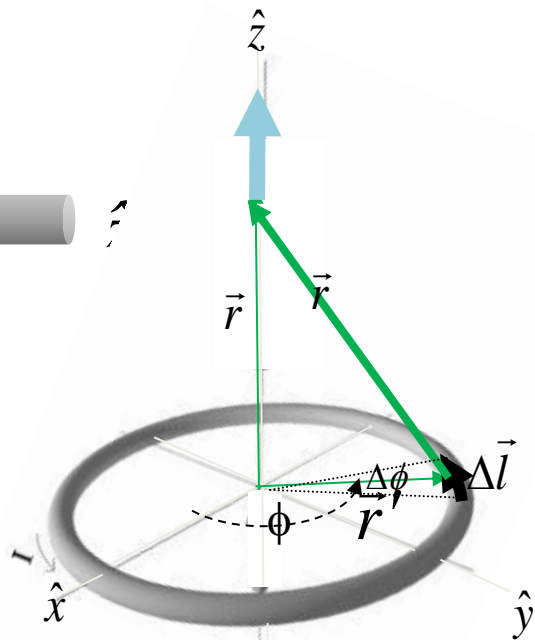
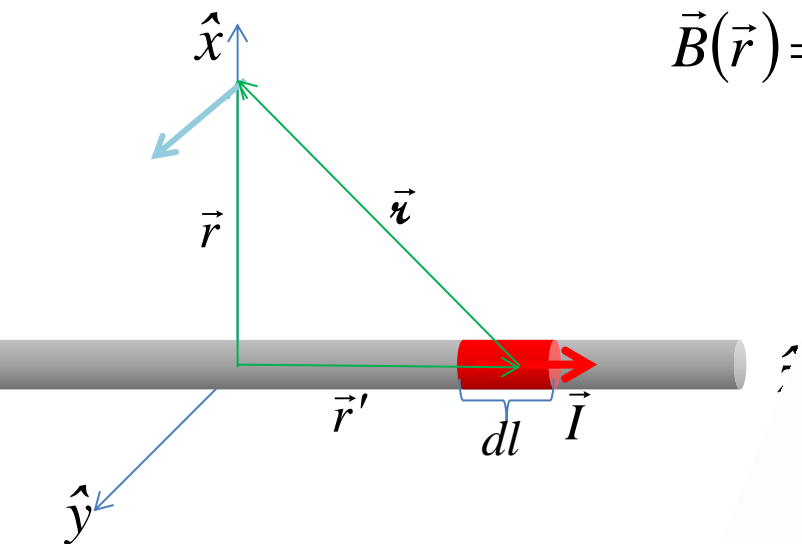
Biot-Savart Law



Magneto-statics

Fields of current distributions

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{I d\vec{\ell}' \times \hat{r}}{r^2}$$

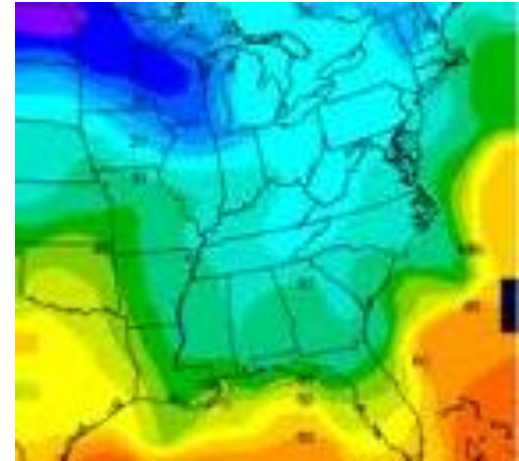


Del Operator

$$\vec{\nabla} \equiv \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z}$$

Gradient – vector representing the local slope of a scalar field.

$$\vec{\nabla} T = \frac{\partial T}{\partial x} \hat{x} + \frac{\partial T}{\partial y} \hat{y} + \frac{\partial T}{\partial z} \hat{z}$$



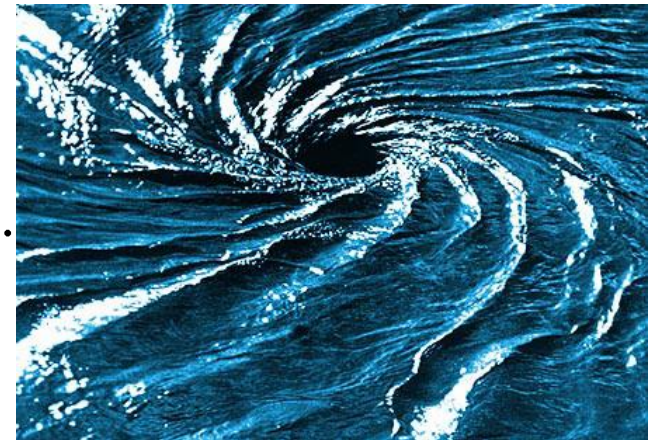
Divergence – scalar representing in/out flow from a point in a vector field.

$$\vec{\nabla} \cdot \vec{v} = \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z}$$



Curl – vector representing circulation of a vector field.

$$\vec{\nabla} \times \vec{v} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ v_x & v_y & v_z \end{vmatrix} = \hat{x} \left(\frac{\partial v_z}{\partial y} - \frac{\partial v_y}{\partial z} \right) + \dots$$



Memory Lane: Electrostatics

Flux from Charge Sources

$$\oint \vec{E}_1 \cdot d\vec{a} = \Phi_{E1}$$

$$\Phi_{E1} = \oint E_1 da_{\parallel}$$

$$\Phi_{E1} = \int_{\phi=-\frac{\pi}{2}}^{\frac{\pi}{2}} \int_{\theta=0}^{2\pi} \frac{q_1}{4\pi\epsilon_0 r^2} r^2 d\phi \sin\theta d\theta$$

$$\Phi_{E1} = \frac{q_1}{4\pi\epsilon_0} 4\pi$$

$$\oint \vec{E}_1 \cdot d\vec{a} = \Phi_{E1} = \frac{q_1}{\epsilon_0}$$

Ditto for q_2, q_3, \dots

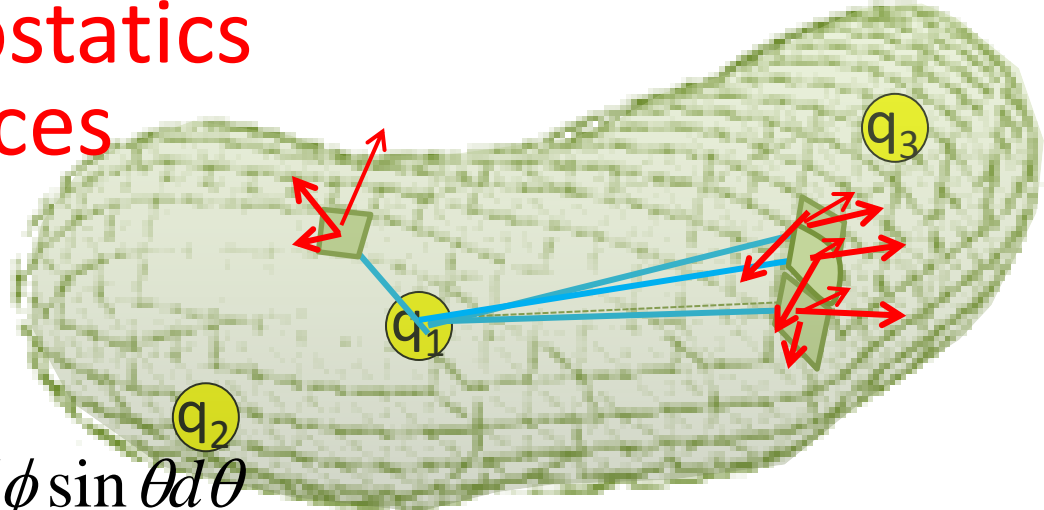
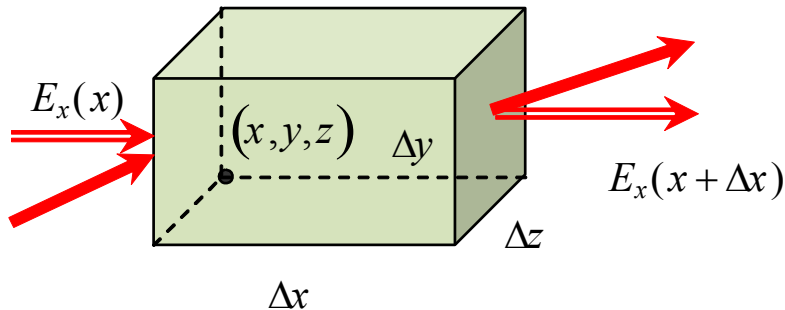
$$\oint \vec{E}_{net} \cdot d\vec{a} = \frac{Q_{net, enclosed}}{\epsilon_0}$$

Simplified symmetric problems

$$\vec{\nabla} \cdot \vec{E} = \frac{1}{\epsilon_0} \rho$$

(integral form) Gauss's Law (derivative form)

Pause & Put together Gauss's Th'm



$$\text{div}(\vec{E}) \equiv \lim_{Vol \rightarrow 0} \frac{\Phi_E}{Vol} = \lim_{Vol \rightarrow 0} \frac{1}{\epsilon_0} \frac{Q_{encl}}{Vol}$$

$$\text{div}(\vec{E}) = \lim_{Vol \rightarrow 0} \frac{\oint \vec{E} \cdot d\vec{a}}{Vol} = \frac{1}{\epsilon_0} \rho$$

$$\oint \vec{E} \cdot d\vec{l} = 0$$

Motivated scalar

$$\text{potential } \Delta V = -\int \vec{E} \cdot d\vec{l}$$

$$\vec{\nabla} \times \vec{E} = 0$$

$$-\vec{\nabla} V = \vec{E}$$

Gauss's Theorem – explicitly putting it together

$$\oint \vec{E} \cdot d\vec{a} = \frac{Q_{\text{enclosed}}}{\epsilon_0} \quad \text{but} \quad Q_{\text{encl}} = \int \rho d\tau \quad \text{And we'd gone off and proven} \quad \vec{\nabla} \cdot \vec{E} = \frac{1}{\epsilon_0} \rho$$

Putting these together:

$$\oint \vec{E} \cdot d\vec{a} = \int \frac{\rho}{\epsilon_0} d\tau$$

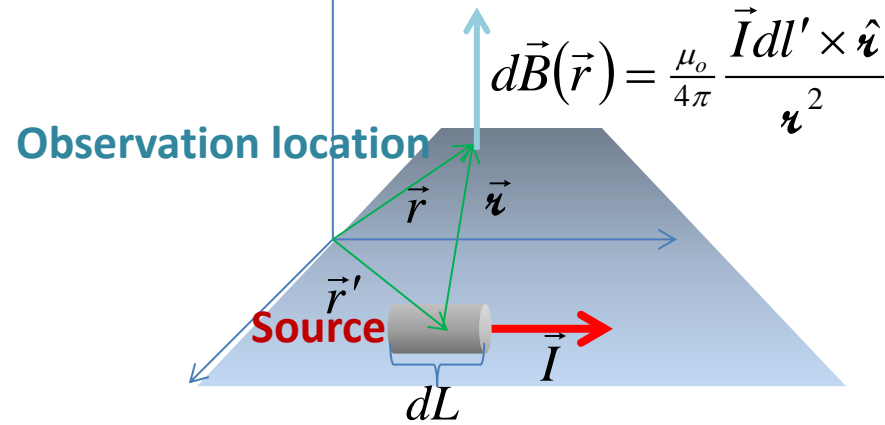
$$\oint \vec{E} \cdot d\vec{a} = \int \vec{\nabla} \cdot \vec{E} d\tau$$

Though we were thinking specifically about electric field while we did the math that got us to this relation, it's quite general and true for any vector field. So, as expressed in Ch. 1, for generic function F ,

$$\oint \vec{F} \cdot d\vec{a} = \int \vec{\nabla} \cdot \vec{F} d\tau$$

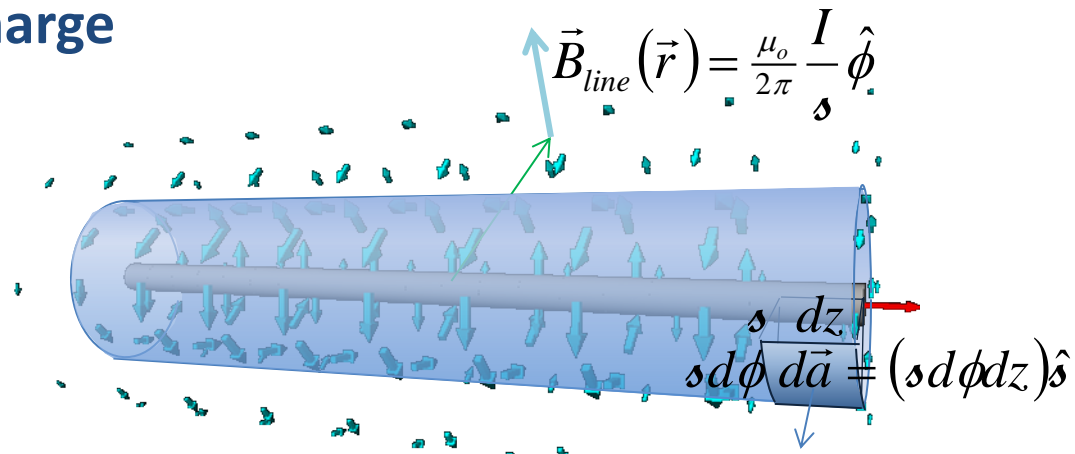
Magneto-Statics

Flux from Current Sources



$$\oint (d\vec{B}(\vec{r})) \cdot d\vec{a} = d\Phi_B = \oint \left(\frac{\mu_0}{4\pi} \frac{\vec{I} dl' \times \hat{n}}{r^2} \right) \cdot d\vec{a}$$

Not so easy; start with special case to *suggest / understand* general result
infinite line charge



Surface of any radius

$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{a} = \Phi_B = \oint \left(\frac{\mu_0}{2\pi} \frac{I}{s} \hat{\phi} \right) \cdot d\vec{a} = \oint \left(\frac{\mu_0}{2\pi} \frac{I}{s} \hat{\phi} \right) \cdot (s d\phi dz) \hat{s} = \oint \left(\frac{\mu_0}{2\pi} I d\phi dz \right) (\hat{\phi} \cdot \hat{s}) = 0$$

would work

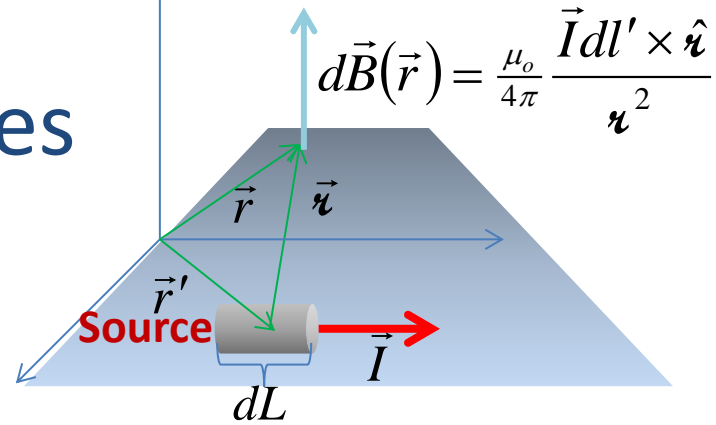
Similarly,

$$\vec{\nabla} \cdot \vec{B}_{line}(\vec{r}) = \frac{1}{s} \frac{\partial}{\partial s} (s B_s) + \frac{1}{s} \frac{\partial}{\partial \phi} (B_\phi) + \frac{\partial}{\partial z} (B_z) = \frac{1}{s} \frac{\partial}{\partial s} (s \cdot 0) + \frac{1}{s} \frac{\partial}{\partial \phi} \left(\frac{\mu_0}{2\pi} \frac{I}{s} \right) + \frac{\partial}{\partial z} (0) = 0$$

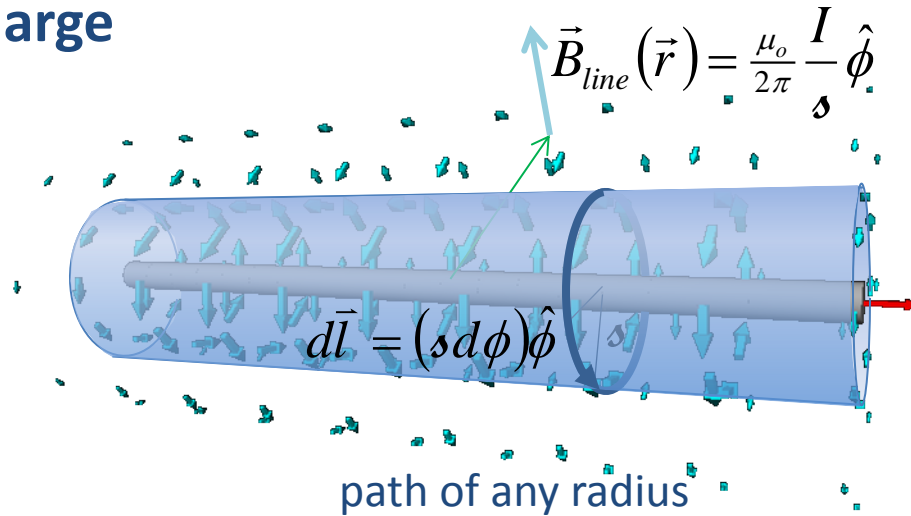
Magneto-Statics

Circulation from Current Sources

$$\oint (d\vec{B}(\vec{r})) \cdot d\vec{l} = \oint \left(\frac{\mu_0}{4\pi} \frac{\vec{I} dl' \times \hat{r}}{r^2} \right) \cdot d\vec{l}$$



Not so easy; start with special case to *suggest / understand* general result
infinite line charge



$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{a} = 0$$

$$\vec{\nabla} \cdot \vec{B}_{line}(\vec{r}) = 0$$

$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{l} = \oint \left(\frac{\mu_0}{2\pi} \frac{I}{s} \hat{\phi} \right) \cdot d\vec{l} = \oint \left(\frac{\mu_0}{2\pi} \frac{I}{s} \hat{\phi} \right) \cdot (s d\phi) \hat{\phi} = \oint \left(\frac{\mu_0}{2\pi} I d\phi \right) (\hat{\phi} \cdot \hat{\phi}) = \frac{\mu_0}{2\pi} I 2\pi = \mu_0 I$$

What of $Curl(\vec{B}_{line}(\vec{r}))$? Takes a little work to get right answer and understand.

Ampere's Law

$$\oint \vec{B} \cdot d\vec{\ell} = \mu_0 I_{\text{piercing}}$$

Goes Differential: Curl

Curl=circulation density (per area encircled)

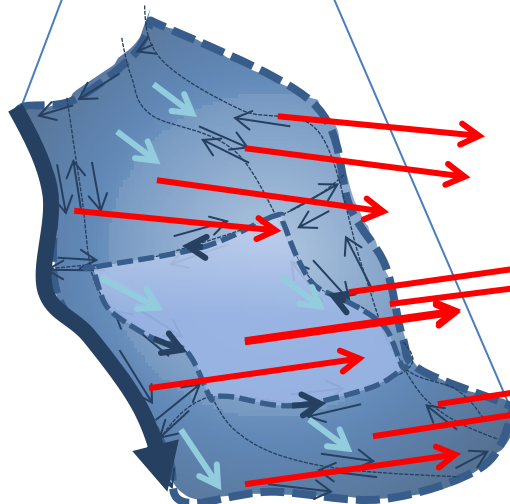
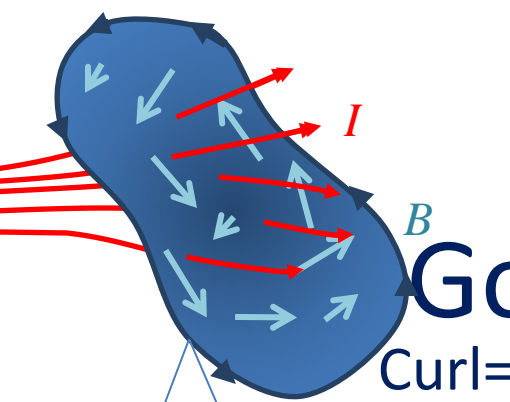
Zoom in to differential scale:

Break area into differential area 'patches'

Break closed path into paths around differential patches

(ultimately all internal path legs cancel with each other)

Project onto coordinate planes



$$[\text{curl}(\vec{B})]_{y.\text{component}} = \dots$$

$$[\text{curl}(\vec{B})]_{x.\text{component}} = \dots$$

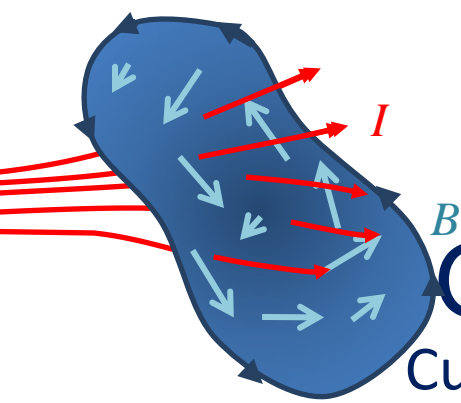
$$[\text{curl}(\vec{B})]_{z.\text{component}} \equiv \lim_{\Delta A_{z.\text{patch}} \rightarrow 0} \left(\frac{\oint \vec{B} \cdot d\vec{\ell}_{z.\text{patch}}}{\Delta A_{z.\text{patch}}} \right)$$

Ampere's Law

$$\oint \vec{B} \cdot d\vec{\ell} = \mu_0 I_{\text{piercing}}$$

Goes Differential: Curl

Curl=circulation density (per area encircled)



$[\text{curl}(\vec{B})]_x = \lim_{\Delta A_{x.\text{patch}} \rightarrow 0} \left(\frac{\oint \vec{B} \cdot d\vec{\ell}_{x.\text{patch}}}{\Delta A_{x.\text{patch}}} \right) = \lim_{\Delta A_{x.\text{patch}} \rightarrow 0} \left(\frac{\mu_0 I_{x.\text{patch}}}{\Delta A_{x.\text{patch}}} \right)$

$[\text{curl}(\vec{B})]_y = \dots$

$[\text{curl}(\vec{B})]_z = \dots$

$$\lim_{\Delta y \Delta z \rightarrow 0} \left[\frac{B_y(z)\Delta y + B_z(y+\Delta y)\Delta z + B_y(z+\Delta z)(-\Delta y) + B_z(y)(-\Delta z)}{\Delta y \Delta z} \right]$$

$$\lim_{\Delta y \Delta z \rightarrow 0} \left[\frac{B_z(y+\Delta y)\Delta z - B_z(y)\Delta z}{\Delta y \Delta z} - \frac{B_y(z+\Delta z)\Delta y - B_y(z)\Delta y}{\Delta y \Delta z} \right]$$

$$[\text{curl}(\vec{B})]_x = \frac{\partial B_z}{\partial y} - \frac{\partial B_y}{\partial z} = \mu_0 \frac{dI_x}{dA_{x.\text{patch}}} = \mu_0 J_x$$

Similarly, $[\text{curl}(\vec{B})]_y = \frac{\partial B_x}{\partial z} - \frac{\partial B_z}{\partial x} = \mu_0 J_y$ and $[\text{curl}(\vec{B})]_z = \frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y} = \mu_0 J_z$

$$\text{curl}(\vec{B}) = \left\langle \frac{\partial B_z}{\partial y} - \frac{\partial B_y}{\partial z}, \frac{\partial B_x}{\partial z} - \frac{\partial B_z}{\partial x}, \frac{\partial B_y}{\partial x} - \frac{\partial B_x}{\partial y} \right\rangle = \mu_0 \langle J_x, J_y, J_z \rangle \quad \text{or} \quad \vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$$

Magneto-Statics

Divergence and Circulation from Current Sources

Derivation specific to constant, Infinite Line-Current

$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{l} = \mu_o I$$

Stokes' Theorem

$$\vec{\nabla} \times \vec{B} = \mu_o \vec{J}$$

$$\vec{B}_{line}(\vec{r}) = \frac{\mu_o}{2\pi} \frac{I}{s} \hat{\phi}$$

$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{a} = 0$$

Gauss's Theorem

$$\vec{\nabla} \cdot \vec{B}_{line}(\vec{r}) = 0$$

Note: both follow from applying Biot-Savart, which holds only for steady currents

Pause and put together Stoke's:

Now for more general (more mathematical / less intuitive) proof

Stoke's Theorem – explicitly putting it together

$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{l} = \mu_o I \quad \text{but} \quad \vec{I} = \int \vec{J} da \quad \text{And we'd gone off and proven} \quad \vec{\nabla} \times \vec{B} = \mu_o \vec{J}$$

Putting these together:

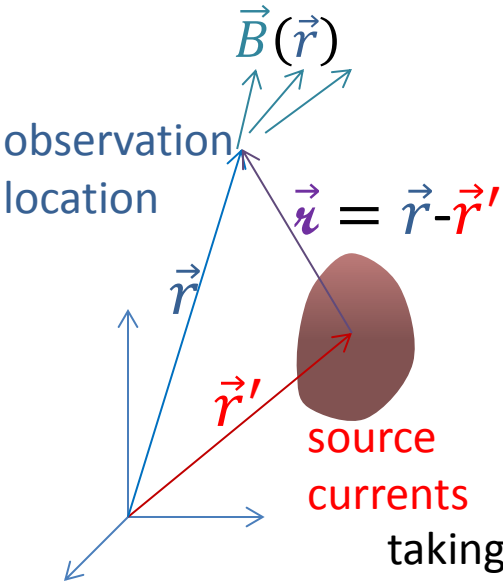
$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{l} = \int \mu_o \vec{J} \cdot da$$

$$\oint \vec{B}(\vec{r})_{line} \cdot d\vec{l} = \int (\vec{\nabla} \times \vec{B}) \cdot da$$

Though we were thinking specifically about magnetic field while we did the math that got us to this relation, it's quite general and true for any vector field. So, as expressed in Ch. 1, for generic function F,

$$\oint \vec{F} \cdot d\vec{l} = \int (\vec{\nabla} \times \vec{F}) \cdot d\vec{a}$$

Derive Ampere's Differential form



$$\vec{\nabla}_r \times \vec{B}(\vec{r}) = \vec{\nabla}_r \times \left(\frac{\mu_0}{4\pi} \int \frac{\vec{J} \times \hat{r}}{r^2} d\tau' \right)$$

using

$$\vec{I} dl' = \frac{\vec{I}}{da_{\perp}} dl' da_{\perp} = \vec{J} d\tau'$$

Can slip del inside integral since *not* taking derivative with respect to integration variable

$$\vec{\nabla}_r \times \vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int \vec{\nabla}_r \times \left(\vec{J} \times \frac{\hat{r}}{r^2} \right) d\tau'$$

Use Product Rule (8): $\vec{\nabla} \times (\vec{A} \times \vec{B}) = (\vec{B} \cdot \vec{\nabla})\vec{A} - (\vec{A} \cdot \vec{\nabla})\vec{B} + \vec{A}(\vec{\nabla} \cdot \vec{B}) - \vec{B}(\vec{\nabla} \cdot \vec{A})$

taking derivative to see how field varies from one observation location to another, not for changes in source locations

$$\vec{\nabla}_r \times \left(\vec{J} \times \frac{\hat{r}}{r^2} \right) = \left(\frac{\hat{r}}{r^2} \cdot \vec{\nabla}_r \right) \vec{J} - (\vec{J} \cdot \vec{\nabla}_r) \frac{\hat{r}}{r^2} + \vec{J} \left(\vec{\nabla}_r \cdot \frac{\hat{r}}{r^2} \right) - \frac{\hat{r}}{r^2} (\vec{\nabla}_r \cdot \vec{J}) = -(\vec{J} \cdot \vec{\nabla}_r) \frac{\hat{r}}{r^2} + \vec{J} \left(\vec{\nabla}_r \cdot \frac{\hat{r}}{r^2} \right)$$

$$\vec{\nabla}_r \times \vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \left(\int -(\vec{J} \cdot \vec{\nabla}_r) \frac{\hat{r}}{r^2} d\tau' + \int \vec{J} \left(\vec{\nabla}_r \cdot \frac{\hat{r}}{r^2} \right) d\tau' \right)$$

$$\vec{\nabla}_r \cdot \frac{\hat{r}}{r^2} = 4\pi \delta^3(\vec{r})$$

Motivation

by Gauss's theorem

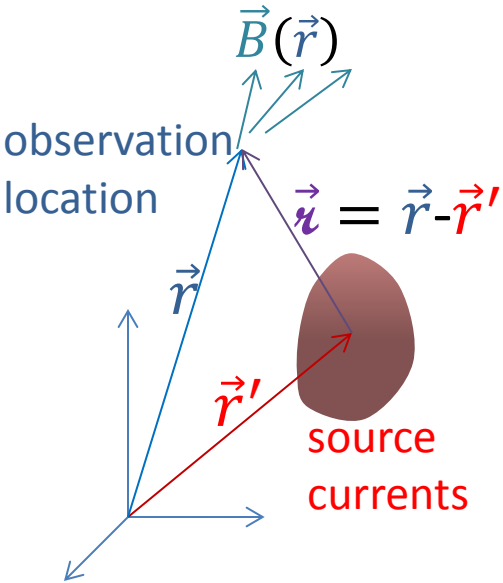
$$\int \left(\vec{\nabla} \cdot \left(\frac{\hat{r}}{r^2} \right) \right) d\tau = \int \left(\frac{\hat{r}}{r^2} \right) \cdot d\vec{a} = \int \left(\frac{1}{r^2} \right) r^2 \sin \theta d\theta d\phi = 4\pi$$

Looking at just one component

$$4\pi \vec{J}(\vec{r})$$

$$\left((\vec{J} \cdot \vec{\nabla}_{r'}) \frac{x-x'}{r^3} \right) \hat{x} = \left(\vec{\nabla}_{r'} \cdot \left(\vec{J} \frac{x-x'}{r^3} \right) - \frac{x-x'}{r^3} (\vec{\nabla}_{r'} \cdot \vec{J}) \right) \hat{x}$$

Derive Ampere's Differential form



$$\vec{\nabla}_r \times \vec{B}(\vec{r}) = \vec{\nabla}_r \times \left(\frac{\mu_o}{4\pi} \int \frac{\vec{J} \times \hat{r}}{r^2} d\tau' \right) \quad \text{using } \vec{I} dl' = \frac{\vec{I}}{da_{\perp}} dl' da_{\perp} = \vec{J} d\tau'$$

$$\vec{\nabla}_r \times \vec{B}(\vec{r}) = \frac{\mu_o}{4\pi} \left(\int (\vec{J} \cdot \vec{\nabla}_{r'}) \frac{\hat{r}}{r^2} d\tau' + 4\pi \vec{J}(\vec{r}) \right)$$

where

$$\left((\vec{J} \cdot \vec{\nabla}_{r'}) \frac{x-x'}{r^3} \right) \hat{x} = \left(\vec{\nabla}_{r'} \cdot \left(\vec{J} \frac{x-x'}{r^3} \right) - \frac{x-x'}{r^3} (\vec{\nabla}_{r'} \cdot \vec{J}) \right) \hat{x}$$

Ditto for other two components

For now, with electro-magnetic *statics*

$$\vec{\nabla}_r \times \vec{B}(\vec{r}) = \frac{\mu_o}{4\pi} (0 + 4\pi \vec{J}(\vec{r}))$$

$$\vec{\nabla}_{r'} \cdot \vec{J} = -\frac{d\rho}{dt} = 0$$

Gauss's theorem

$$\vec{\nabla}_r \times \vec{B}(\vec{r}) = \mu_o \vec{J}(\vec{r})$$

$$\int \vec{\nabla}_{r'} \cdot \left(\vec{J} \frac{x-x'}{r^3} \right) d\tau' = \int \left(\vec{J} \frac{x-x'}{r^3} \right) \cdot d\vec{a}' = 0$$

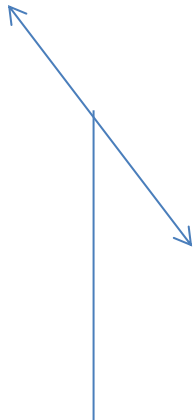
So by Stokes' Theorem

If area *fully encloses* current, then no current penetrates area

$$\oint \vec{B}(\vec{r}) \cdot d\vec{l} = \mu_o \int \vec{J}(\vec{r}) \cdot d\vec{a}' = \mu_o I$$

Ditto for other two components

Maxwell's laws for electro-statics

$$\begin{array}{ll} \vec{\nabla}_r \times \vec{B}(\vec{r}) = \mu_0 \vec{J}(\vec{r}) & \vec{\nabla}_r \times \vec{E}(\vec{r}) = 0 \\ \text{Ampere's } \oint \vec{B}(\vec{r}) \cdot d\vec{l} = \mu_0 I & \oint \vec{E}(\vec{r}) \cdot d\vec{l} = 0 \\ \vec{\nabla}_r \cdot \vec{B}(\vec{r}) = 0 & \vec{\nabla}_r \cdot \vec{E}(\vec{r}) = \frac{1}{\epsilon_0} \rho(\vec{r}) \\ \int \vec{B}(\vec{r}) \cdot d\vec{a} = 0 & \int \vec{E}(\vec{r}) \cdot d\vec{a} = \frac{1}{\epsilon_0} Q \quad \text{Gauss's} \end{array}$$


For arguably symmetric fields,
useful for finding fields

Wed.	(C 21.6-7,.9) 1.3.4-1.3.5, 1.5.2-1.5.3, 5.3.1-.3.2 Div & Curl B	
Fri.	(C 21.6-7,.9) 5.3.3-.3.4 Applications of Ampere's Law	
Mon.	1.6, 5.4.1-.4.2 Magnetic Vector Potential	HW8
Wed.	5.4.3 Multipole Expansion of the Vector Potential	
Thurs.		
Fri.	Review	